Identification of CaSO₄ Formed by Reaction of CaO and SO₂

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The injection of calcium-based sorbents into coal-fired boilers for reaction with, and reduction in the levels of, sulfur dioxide (SO₂) in the flue gas has undergone considerable research and development. Significant effort has also been made in developing models for the overall reaction

$$CaO + SO_2 + 1/2 O_2 \leftrightarrow CaSO_4$$

in order to better predict the effects of system and sorbent variables upon performance. Development of internal surface area (Borgwardt and Bruce, 1986) and pore structure (Hartman and Coughlin, 1974) is necessary for measurable reaction to occur. Further, since the calcium sulfate (CaSO₄) product has a larger molar volume than the reactant, calcium oxide (CaO), the extent of pore volume development may control the levels of reaction. The molar volume of CaSO₄ is related to its density. One of the earlier references (Hartman and Coughlin, 1974) to the CaSO₄ product density uses the molar volume value of 52.2 cm³/mol or 2.6 g/cm³. This leads to a product/reactant expansion ratio,

$$Z = v_{\text{CaSO}_4} / v_{\text{CaO}}$$
,

of 52.2/16.9, or 3.09. Use of this particular handbook value (Weast, 1968) of density (or its associated Z value) has continued in subsequent papers (Hartman and Coughlin, 1976; Ramachandran and Smith, 1977; Hartman et al., 1978; Bhatia and Perlmutter, 1981; Sotirchos and Yu, 1985; Reyes and Jensen, 1987; Borgwardt et al., 1987; Kocaefe et al., 1987; Simons and Garman, 1986; Yu and Sotirchos, 1987). One instance (Hartman and Trnka, 1980) is noted where the value of 2.97 g/cm³ (45.8 cm³/mol) has been used, cited from an unidentified

handbook. This last case results in a Z value of 2.71. Apparently the earliest documented reference questioning the commonly-accepted molar volume value is by Dam-Johansen (1987). This work determined a molar volume of 48.06 cm³/mol from a model comparison with experimental porosity/conversion data. Deviation from the inferred 46.0 cm³/mol (2.96 g/cm³) value was attributed to experimental errors and an insufficient model.

The value of Z is significant particularly for modeling the sulfation reaction. Since the larger volume product fills or blocks sorbent pore volume, slowing or stopping the reaction, the ability of models to appropriately simulate laboratory reaction results is contingent upon proper determination of the physical parameters involved. To this end, analyses to identify the form of the CaSO₄ product and determine its density (molar volume) were performed.

Experimental Method

Samples of calcium hydroxide [Ca(OH)₂] and calcium carbonate (CaCO₃) were reacted at 800°C for 5 min supported on quartz wool in a fixed-bed reactor. Preheated reactor gas [0.3% SO₂, 5% oxygen (O₂), balance nitrogen (N₂)] at 23 L/min and standard temperature and pressure (STP) passed through the sample bed, converting the sample to the reactive CaO form and then partially reacting it to form CaSO₄. (Further details of similar experimental procedures are available in Borgwardt and Bruce, 1986.) The samples were analyzed by x-ray diffraction (XRD), helium pycnometry, atomic absorption spectroscopy (AA), ion chromatography (IC), and thermogravimetric analysis (TGA).

XRD analyses for compound identification were performed on a diffractometer with a copper $K\alpha$ target source running at 50 kV and 40 mA. The entrance aperture was 1.0 degree and the

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detector slit was 0.05 degree. Spectra were identified by computer comparison with the Joint Committee for Powder Diffraction Spectra (JCPDS) spectral files. Density measurements were performed on a helium pycnometer which measures solid sample volume. Calibration with manufacturer-supplied standards ensured instrument accuracy and precision. TGA measurements determined the weight percent of trace Ca(OH)₂ and CaCO₃ in the sample product, while AA and IC measurements determined the weight percent of SO₄ and Ca⁺⁺, respectively.

Results and Discussion

Figure 1 shows the XRD spectrum of the sample product formed from the reaction of Ca(OH)₂ with SO₂. This spectrum is overlaid with the spectrum for CaO to account for incomplete conversion to product CaSO₄. The XRD spectrum from the CaCO₃ sample product was nearly identical to that from the Ca(OH)₂ sample product, except for slightly higher CaO peaks. The higher CaO peaks are due to the longer time for calcination of the CaCO₃ than dehydration of the Ca(OH)₂. For both calcium-based precursors, the analysis identified the sample product to be calcium sulfate anhydrite, JCPDS registry No. 37-1496. This is an orthorhombic crystal structure with a density of 2.995 g/cm³ (45.46 cm³/mol). Figure 1 shows that the CaO and CaSO₄ spectra account for all major and minor peaks present in the sample spectrum, affirming the identity of the CaSO₄ product.

The identification of this CaSO₄ form, having a higher density than previously ascribed to the CaSO₄ product, led to further efforts to verify the density. Since the XRD spectra identified the same CaSO₄ for both CaCO₃ and Ca(OH)₂ sorbents, helium pycnometer analyses were done only on the reaction product of Ca(OH)₂. TGA, AA and IC results (accounting for 99.5% of the sample product mass) determined the Ca(OH)₂, CaO, CaCO₃ and CaSO₄ composition of the reacted product. These results, when combined with the helium pycnometry analyses, determined the sample density. The results from five trials indicate a compound with a mean density of 2.98 g/cm³ (standard deviation of 0.08).

Figure 2 shows the impact of this density determination upon

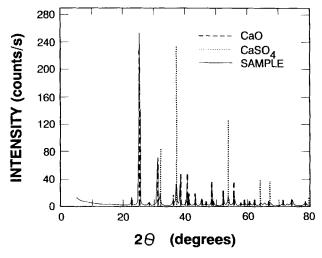


Figure 1. XRD spectra of Ca(OH)₂ sulfation sample with CaO spectra (JCPDS No. 37-1497) and CaSO₄ anhydrite spectra (JCPDS No. 37-1496).

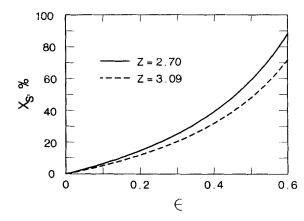


Figure 2. Maximum conversion based on complete filling of initial porosity with Z = 3.09 and 2.70.

pore-volume-limited sulfation of the CaO and compares it with the more commonly-used density value. The molar volume ratio Z, 2.70, calculated from the density determined in this work, suggests that considerably more reaction can occur within the porous matrix than with the commonly-cited value of 3.09. For $Ca(OH)_2$ that develops its theoretical porosity during dehydration to CaO, its theoretical porosity, ϵ , is

$$1 - \nu_{CaO}/\nu_{Ca(OH)_2}$$
= 1 - 16.9 cm³/mol/33.1 cm³/mol = 0.489.

Likewise, for calcination of $CaCO_3$, ϵ is

$$1 - \nu_{\text{CaO}} / \nu_{\text{CaCO}_3}$$
= 1 - 16.9 cm³/mol/36.9 cm³/mol = 0.542.

These molar volume values are derived from Weast (1968). The maximum conversion based upon complete pore filling of the porosity by the larger volume product can be calculated from

$$X_s = \epsilon/(Z-1)(1-\epsilon)$$

Thus, the maximum expected conversion for $Ca(OH)_2$ is 56.3% and for $CaCO_3$ is 69.6%.

While this Z value helps to account for some of the excesses of the X_s values noted experimentally (Kocaefe et al., 1987; Gullett et al., 1988), it does not fully account for reaction levels (up to 90% conversion) observed by Borgwardt and Bruce (1986). Nonetheless, the magnitude of the density change will have a significant effect upon sulfation models that incorporate reaction limitations based upon pore filling or blocking.

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Notation

 ϵ = original porosity

 $\nu_{\text{CaO}} = \text{molar volume of CaO}, \text{cm}^3/\text{mol}$

 $\nu_{\text{CaSO}_4} = \text{molar volume of CaSO}_4, \text{cm}^3/\text{mol}$

- X_s = conversion to product based on complete pore volume filling,
- $Z = \text{molar volume ratio of CaSO}_4/\text{CaO}$
- 2Θ = angle of detector to x-ray beam, deg

Literature Cited

- Bhatia, S. K., and D. D. Perlmutter, "The Effect of Pore Structure on Fluid-Solid Reactions: Application to the SO₂-Lime Reaction," *AIChE J.*, 27, 226 (Mar., 1981).
- Borgwardt, R. H., and K. R. Bruce, "Effect of Specific Surface Area on the Reactivity of CaO with SO₂," AIChE J., 32, 239 (Feb., 1986).
- Borgwardt, R. H., K. R. Bruce, and J. Blake, "An Investigation of Product-Layer Diffusivity for CaO Sulfation," I & E C Res., 26, 1993 (1987).
- Dam-Johansen, K., "Sulphur Dioxide Retention on Dry Chalk," PhD Thesis, Technical Univ. of Denmark, Lyngby (1987).
- Gullett, B. K., J. A. Blom, and R. T. Cunningham, "Porosity, Surface Area, and Particle Size Effects of CaO Reacting With SO₂ at 1,100°C," React. Solids, 6, 263 (1988).
- Hartman, M., and R. W. Coughlin, "Reaction of Sulfur Dioxide with Limestone and the Influence of Pore Structure," I & E C Process Des. Dev., 13, 248 (1974).
- Hartman, M., and R. W. Coughlin, "Reaction of Sulfur Dioxide with Limestone and the Grain Model," *AIChE J.*, **22**, 490 (May, 1976).

- Hartman, M., J. Pata, and R. W. Coughlin, "Influence of Porosity of Calcium Carbonates on Their Reactivity with Sulfur Dioxide,"

 1.8 F. C. Process Des. Dev. 17, 411 (1978)
- I & E C Process Des., Dev., 17, 411 (1978).
 Hartman, M., and O. Trnka, "Influence of Temperature on the Reactivity of Limestone Particles With Sulfur Dioxide," Chem. Eng. Sci., 35, 1189 (1980).
- Kocaefe, D., D. Karman, and F. R. Steward, "Interpretation of the Sulfation Rate of CaO, MgO, and ZnO with SO₂ and SO₃," *AIChE J.*, 33, 1835 (Nov., 1987).
- Ramachandran, P. A., and J. M. Smith, "A Single Pore Model for Gas-Solid Noncatalytic Reactions," AIChE J., 23, 353 (May, 1977).
- Reyes, S., and K. F. Jensen, "Percolation Concepts in Modelling of Gas-Solid Reactions: III. Application to Sulphation of Calcined Limestone," Chem. Eng. Sci., 42, 565 (1987).
- Simons, G. A., and A. R. Garman, "Small Pore Closure and the Deactivation of the Limestone Sulfation Reaction," *AIChE J.*, 32, 1491 (Sept., 1986).
- Sotirchos, S. V., and H-C Yu, "Mathematical Modelling of Gas-Solid Reactions with Solid Product," Chem. Eng. Sci., 40, 2039 (1985).
 Yu, H-C., and S. V. Sotirchos, "A Generalized Pore Model for Gas-
- Yu, H-C., and S. V. Sotirchos, "A Generalized Pore Model for Gas-Solid Reactions Exhibiting Pore Closure," AIChE J., 33, 382 (Mar., 1987).
- Weast, R. C., Handbook of Chemistry and Physics, 49th ed., The Chemical Rubber Co., Cleveland, OH (1968).

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